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# Kinetics Study and Process Optimization for the Reaction of Carbohydrazide with Sodium Percarbonate

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**Abstract:** Zinc tri(carbohydrazide) perchlorate(GTX) is a widely-used, safe, environmental-friendly and highly-energetic primary explosive. However, excessive quantities of carbohydrazide(CHZ) and GTX are dissolved in the mother liquor during the primary explosive manufacturing processes. To maximize the elimination of the residual CHZ, the reaction process and influence factors of the reaction of sodium percarbonate(SPC) with CHZ were studied by using the volumetric titration analysis and the controlled variable method. The optimum reaction conditions under 80  $^{\circ}$ C are as follows: the volume ratio of CHZ (0.1 mol  $^{\circ}$ L<sup>-1</sup>) and SPC (0.15 mol  $^{\circ}$ L<sup>-1</sup>) is 1 : 4, the reaction time isn't less than 90 min, and the corresponding removal rate of CHZ could be as high as 68%. Moreover, the obtained reaction time and the residual CHZ concentration were fitted by the least square method based on both first-order and second-order kinetic models. Results indicate that the aforementioned reaction accords with the second-order kinetic model.

Key words: carbohydrazide(CHZ); sodium percarbonate(SPC), titration analysis

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#### 1 Introduction

Nowadays, many domestic enterprises show great interest in the zinc (  $\rm II$  ) tri(carbohydrazide) perchlorate ( GTX) of which is a new, highly-energetic and environmental friendly primary explosive. It is good enough to be applied in civil detonators. However, there are still some residues remaining in the mother liquor such as dissolved GTX, carbohydrazide (CHZ) and perchlorates according to the technical routine  $\rm ^{[1]}$ .

CHZ is a urea derivative, in which both the amide groups of urea are replaced by hydrazine(HZ). It can coordinate with many kinds of metal ions as a monodentate or multidentate  $^{[2-4]}$  since it contains several function groups that possess lone electron pairs. Due to its strong reducibility, CHZ has also been used to design a variety of energetic coordination compounds such as cadmium tri (carbohydrazide) perchlorate of which has been successfully prepared and proved to be remarkable in practical applications. These coordination compounds could act as primary explosives and components in propellants or high explosives  $^{[6-10]}$ .

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GTX has been widely used in civil explosive enterprises now. And after a long period of GTX manufacture period, there is a large amount of CHZ remaining in its mother liquor of which is discharged as waste water. Since CHZ can react with the iron and perchloric acid very easily to form iron tri (carbohydrazide) perchlorate, an extremely sensitive compound that spontaneously explodes in solution. So it is necessary to remove or consume CHZ totally before discharging the waste water. In addition, CHZ is a dangerous grade chemical substance, with a dangerous level of  $5-22-33-41-553^{[10]}$ . The number 53 of 5-22-33-41-553 indicates a long-term detrimental effect on water environment. If the mass of toxic waste was poured outside, the natural living body would be harmed. In order to promote the application of GTX around the world widely, it is imperative to solve the problem of explosive waste water fundamentally during the GTX production processes. Thus, a practical and effective method of destroying CHZ should be developed.

Sodium percarbonate (SPC,  $2Na_2CO_3 \cdot 3H_2O_2$ , M=314.02) is an oxidant carbonate, which can react in solid state with reductants. The reaction exhibits complex multistep behaviors controlled by physic-geometrical and successive chemistry reaction schemes [12-14, 15-21]. The thermal decomposition of SPC can be empirically described as two overlapped reaction steps of endothermic and exothermic processes, which are separated by the physic- geometrical constraints and the changes in the self-generated reaction conditions. In addition, the thermal decomposition of SPC is considered as a suc-

cessive process of the detachment and subsequent decomposition of  $H_2O_2(g)^{[22]}$ . SPC is widely used in industries and laboratories as an effective oxidizing agent and a source of hydrogen peroxide. Due to stable, inexpensive, non-toxic, and easily handled characteristics, this chemical material is extensively used in detergent industry as a bleaching agent. Moreover, SPC has also been utilized in organic synthesis for oxidation reaction [23–24]. Herein, to explore the optimum parameters for the reaction between carbohydrazide and sodium percarbonate, classical chemical titration analysis was used to test the residue concentration of CHZ. A better technology for the reaction of CHZ and SPC was proposed by changing the volume ratio, concentration of SPC and the reaction time with the method of controlling variables.

# 2 Experimental

#### 2.1 Materials and Equipment

CHZ, SPC, potassium iodate, trichloromethane, hydrochloric acid, transfer pipette (25.00 mL), measuring cylinder (50 mL 5 mL) and acid burette (25.00 mL) were commercially obtained from Beijing Tong Guang Fine Chemical Company. All the solvents and reagents were analytical grade and used without further purification.

### 2.2 Experiment Procedure

#### 2.2.1 Reactant Ratio

The titration principle of the mixed solutions with potassium iodate is carried out according to the redox equation (1):  $2KIO_3+N_4H_6CO+4HCI \longrightarrow 2KCI+2ICI+2N_2+CO_2+5H_2O$  (1)

The Jamieson iodate method for the quantitative determination of hydrazine and its salts has also been successfully applied to the estimation of primary hydrazino groups in some compounds, such as hydrazide<sup>[25]</sup>.

9.0080 g (0.1 mol) of CHZ was dissolved in 250 mL deionized water in a beaker and transferred into a 1 L volumetric flask. The beaker and glass bar were rinsed for three times with deionized water. Then, deionized water was added into the volumetric flask to the scale mark. Similarly, 7.8505 g (0.025 mol) of SPC was disposed to obtain 0.1 mol· $L^{-1}$  SPC solution.

There were five steps in the first experiment. Firstly, 50 mL of 0.1 mol  $\cdot$  L<sup>-1</sup> CHZ solution was added into 300 milliliter beaker. Then, 50 mL of 0.1 mol  $\cdot$  L<sup>-1</sup> SPC solution was added. The next, four glasses of 50 mL CHZ solutions were mixed with 100 mL 0.1 mol  $\cdot$  L<sup>-1</sup> SPC, 150 mL 0.1 mol  $\cdot$  L<sup>-1</sup> SPC, 200 mL 0.1 mol  $\cdot$  L<sup>-1</sup> SPC and 250 mL 0.1 mol  $\cdot$  L<sup>-1</sup> SPC, respectively.

All of the five solutions were stirred at 80  $^{\circ}$ C for 30 min. After the reaction, 100 mL of each reacted solutions were

taken into five 250 mL volumetric flasks, and the deionized water was added to the scale mark. The solutions were calibrated to the scale with deionized water, respectively. So the solutions were all diluted 2.5 times. At last, the solutions were tested according to the titration process.

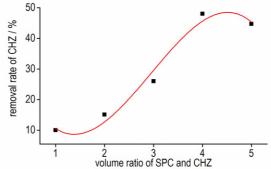
The titration process: 25.00 mL sample solution was transferred into a 250 mL conical flask with a 25.00 mL pipette. Then, 50.00 mL of 10% (mass percent) hydrochloric acid solution was added. After the temperature of the solution was close to room temperature, the solution was titrated with 0.05 mol  $\cdot$  L<sup>-1</sup> potassium iodate standard solution until the solution color changed from brown to light yellow. Then, 5.00 mL of trichloromethane was added into the titration reaction solution again, which was then titrated slowly with heavily shaking until the orange color of the chloroform layer disappeared. All the samples were titrated repeatedly three times in the same manner.

The average consumption of potassium iodate and the reduction ratio was obtained and listed in Table 1. The change curve for the removal rate of CHZ with the volume ratio of CHZ and SPC was shown in Fig.1.

Results indicated that 50 mL of 0.1 mol  $\cdot$  L<sup>-1</sup> CHZ solution mixed with 200 mL of 0.1 mol  $\cdot$  L<sup>-1</sup> of SPC solution possessed the highest removal rate of CHZ (48%). Therefore, the reaction was proved to be very effective when the reactant volume was 50 mL (mol  $\cdot$  L<sup>-1</sup>) CHZ to 200 mL (mol  $\cdot$  L<sup>-1</sup>) SPC. So the solution volume ratio was determined as 1 : 4.

**Table 1** Effects of different reaction material ratio on the consumption of potassium iodate and the removal rate of CHZ

volune of sodium percarbonate /mL	concentration of CHZ /mol·L <sup>-1</sup>	consumption volume of potassium iodate/mL	residue of CHZ /mol·L <sup>-1</sup>	removal rate
50	0.050	18.00	0.0450	10.0
100	0.033	11.20	0.0280	15.1
150	0.025	7.40	0.0185	26.0
200	0.020	4.16	0.0104	48.0
250	0.017	3.75	0.0094	44.7



**Fig.1** The change curve for the removal rate of CHZ to the volume ratio of SPC and CHZ

#### 2.2 The Concentration of SPC Solution

From the procedure 2.2.1, the optimum reactant ratio was obtained as 50 mL of CHZ solution with 200 mL of SPC solution. Thus, the effect of SPC concentrations on the reaction was carried out in this experiment. After controlling the fixed concentration (0.1 mol  $\cdot$  L<sup>-1</sup>) of CHZ, SPC concentration was changed in order to explore the best concentration of SPC.

8.6356, 9.4206, 10.2057, 10.9907 g and 11.7758 g of SPC were dissolved into five beakers, respectively. These solutions were transferred into five 250 mL volumetric flasks, and enough deionized water was poured into the flasks to the scale mark respectively. So 0.11 mol  $\cdot$  L<sup>-1</sup>, 0.12 mol  $\cdot$  L<sup>-1</sup>, 0.13 mol  $\cdot$  L<sup>-1</sup>, 0.14 mol  $\cdot$  L<sup>-1</sup>, 0.15 mol  $\cdot$  L<sup>-1</sup> SPC solutions were well prepared.

There were also five steps in the experiment.

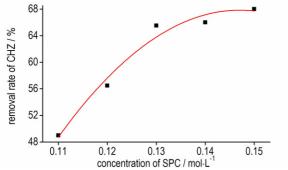
Firstly, 50 mL of 0.1 mol  $\cdot$  L<sup>-1</sup> CHZ solution was added into a 300 milliliter beaker, 200 mL of 0.11 mol  $\cdot$  L<sup>-1</sup> SPC solution was added. In the same way, five glasses of 50 mL 0.1 mol  $\cdot$  L<sup>-1</sup> CHZ solution were mixed with 200 mL 0.12, 0.13, 0.14 mol  $\cdot$  L<sup>-1</sup> and 0.15 mol  $\cdot$  L<sup>-1</sup> SPC solutions respectively.

All of the five mixtures were stirred at 80  $^{\circ}$ C for 30 min. Then, all of the five solutions were taken into five 250 mL volumetric flasks respectively.

The five solutions were titrated in the same way as the same as procedure 2.2.1. The consumption of potassium iodate solution and the reduction ratio were obtained and listed in Table 2. The change curve for the removal rate of CHZ with the different concentration of SPC was listed in Fig.2.

**Table 2** Effects of different SPC concentrations on the consumption of potassium iodate and the removal rate of CHZ

sodium percarbonate /mol·L <sup>-1</sup>	consumption of potassium iodate/mL	residue of CHZ $/\text{mol} \cdot \text{L}^{-1}$	removal rate /%
0.11	10.20	0.0102	40.0
0.11	10.20	0.0102	49.0
0.12	8.70	0.0087	56.5
0.13	6.90	0.0069	65.5
0.14	6.80	0.0068	66.0
0.15	6.40	0.0064	68.0



**Fig.2** The change curve for the removal rate of CHZ to the different concentration of SPC

The results showed that 50 mL of 0.1 mol  $\cdot$  L<sup>-1</sup> CHZ solution mixed with 200 mL of 0.15 mol  $\cdot$  L<sup>-1</sup> SPC solution possessed the highest removal rate of 68%. Therefore, results indicated that the removal rate of CHZ increases with the rise of SPC's concentration (from 0.11 mol  $\cdot$  L<sup>-1</sup> to 0.15 mol  $\cdot$  L<sup>-1</sup>) when the volume ratio (1:4) was curtained. The best concentration of SPC should be controlled in 0.15 mol  $\cdot$  L<sup>-1</sup>.

#### 2.3 Reaction Time

From the procedure 2.2.1 and 2.2.2, a better volume ratio of CHZ solution and SPC solution was obtained as 1:4. The removal rate increases with the increase of SPC's concentration (from 0.11 mol  $\cdot$  L<sup>-1</sup> to 0.15 mol  $\cdot$  L<sup>-1</sup>). The effects of reaction time on the CHZ consumption was explored at the optimized reaction conditions .

Eight glasses of 50 mL of 0.1 mol  $\cdot$  L<sup>-1</sup> CHZ solutions were mixed with eight 200 mL of 0.15 mol  $\cdot$  L<sup>-1</sup> SPC solutions. The mixtures were stirred at 80  $^{\circ}$ C for 20, 30, 40, 50, 60, 90, 120, 150 min respectively.

After the reaction, all of the solutions were taken into five 250 mL volumetric flasks, respectively.

All of the solutions were titrated according to the procedure 2.2.1. The consumption of potassium iodate and the reduction ratio were obtained and listed in Table 3. The change curve for the removal rate of CHZ with different time was listed in Fig.3.

**Table 3** Effects of different reaction time on the consumption of potassium iodate and the removal rate of CHZ

time /min	consumption of potassium iodate/mL	residue of CHZ $/\text{mol} \cdot \text{L}^{-1}$	removal rate/%
20	12.30	0.0123	38.5
30	11.40	0.0114	43.0
40	11.20	0.0112	44.0
50	10.75	0.0108	46.3
60	10.48	0.0105	47.6
90	8.10	0.0081	62.8
120	7.45	0.0075	62.0
150	8.10	0.0081	59.5

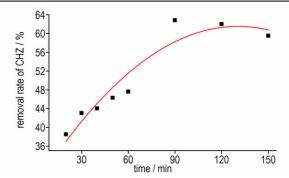


Fig.3 The change curve for the removal rate of CHZ with different time

Results showed that when the volume ratio (1:4) and the concentration (0.1 mol  $\cdot$  L<sup>-1</sup> CHZ and 0.15 mol  $\cdot$  L<sup>-1</sup> SPC) were curtained, the removal rate of CHZ increased with the increasing of reaction time. The best reaction duration should be no less than 90 min.

#### 3 Results and Discussions

All the titration operations were carried out in triplicate. And the results were calculated based on data from blank experiments. The data of all the experiments are real and exact, which indicated a better volume ratio is 1 : 4, a better concentration of SPC is  $0.15~\text{mol} \cdot \text{L}^{-1}$ , and the best reaction time is at least 90 min.

Kinetics studies can be carried out according to the concentration of the residue in CHZ solution. Linear regression method was used to determine the best-fitting kinetic models.

The first order kinetics rate equations can be written in integral the equation as  $^{[26-28]}$ :

$$\frac{\mathrm{d}q_t}{\mathrm{d}t} = k_1 (q_e - q_t) \tag{2}$$

Where, t is reaction time, min;  $q_e$  is the amount of reaction concentration of CHZ at equilibrium, mg  $\cdot$  g<sup>-1</sup>;  $q_t$  is the amount of reaction concentration of CHZ at any time, mg  $\cdot$  g<sup>-1</sup>;  $k_1$  stands for the first order rate constant, min<sup>-1</sup>.

When: t=0,  $q_t=0$ ; which has a linear form of:  $\ln(q_e-q_t) = \ln q_e - k_1 t$ (3)

The second order kinetic model can be written in integral the equation  $as^{[29-30]}$ :

$$\frac{\mathrm{d}q_t}{\mathrm{d}t} = k_2 (q_e - q_t)^2 \tag{4}$$

Where,  $k_2$  stands for the second order rate constant,  $g \cdot (mg \cdot min)^{-1}$ ,

When: t=0,  $q_t=0$ ; which has a linear form of:

$$\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{1}{q_e} t \tag{5}$$

The first order rate constants can be determined experimentally by plotting  $\ln(q_e - q_t)$  against t. Similarly, the second order rate constants can be determined by plotting  $t/q_t$  against t.

According to the linear least-squares method, the first order and the second order kinetic equations were summarized and the parameters obtained by treating CHZ data were listed in Table 4, ( $\Delta m$  represents the amount of CHZ on reaction, mg,) which are the parameters of first and second order kinetics model.

The linear coefficient  $R^2$  of the first order was 0.9558, and the linear coefficient  $R^2$  of the second order was 0.9841. Obviously, fitting all the experimental data with the second order kinetic model was better.

Table 4 Kinetic parameters obtained by treating CHZ data

time	$\Delta m$	$q_t$	$ln(q_e - q_t)$	$(t/q_t)$	first-order kinetic equation	second order kinetic equation
/min	/mg	$/\mathrm{mg}\cdot\mathrm{g}^{-1}$	\ Te Tt /	$/\min \cdot g \cdot mg^{-1}$		
20	173.404	18.4069	2.3066	1.0866	$\ln(q_e - q_t) = -0.0136t + 2.5341$	$t/q_t = 0.0300t + 0.6220$
30	193.672	20.5584	2.0654	1.4593	$m(q_e   q_t) = 0.0130t12.3341$	$t/q_t = 0.0300t \cdot 0.0220$
40	198.176	21.0365	2.0030	1.9015		
50	208.310	22.1122	1.8461	2.2612	$k_1(\min^{-1}) = 0.0136$	$k_2( g \cdot mg^{-1} \cdot min) = 0.0015$
60	214.390	22.7577	1.7386	2.6365	C/,	
90	267.988	28.4470	$q_e$	3.1638	) *	
120	281.500	29.8813	-	4.0159	$R_1^2 = 0.9558$	$R_2^2 = 0.9841$
150	267.988	28.4470	-	5.2730		

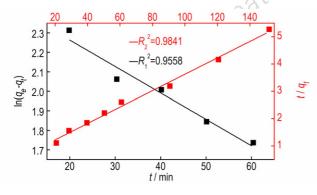


Fig.4 The first and second order kinetic model analysis curves for the reaction of CHZ with SPC in solution

# 4 Conclusions

- (1) It is the first time to obtain the optimal reaction conditions of CHZ and SPC and the chemical kinetics equation and its curves. All of these make significant contributions to the removal of CHZ in the GTX solutions.
- (2) When the solution volume ratio of CHZ (0.1 mol  $\cdot$  L<sup>-1</sup>) and SPC (0.1 mol  $\cdot$  L<sup>-1</sup>) was kept at the range from 1 to 4, the reaction proved to be very sufficient.
- (3) When the reactant ratio (1:4) was curtained, the removal rate of CHZ increased with the increase of the SPC's concentration in solution (from 0.11 mol  $\cdot$  L<sup>-1</sup> to 0.15 mol  $\cdot$  L<sup>-1</sup>). And the best concentration is 0.15 mol  $\cdot$  L<sup>-1</sup>.
  - (4) The removal rate of CHZ increased with the delay of

mixing reaction time. And the optimum time is at least 90 min. The-second-order linear kinetics model reaches the highest linear fitting degree for the reaction of CHZ with SPC.

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# 碳酰肼和过碳酸钠反应的化学动力学和反应工艺

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溶解有过量的 内(SPC 摘 要: 高氯酸三碳酰肼合锌(GTX)是一种大量使用的安全环保型高能起爆药,其母液中溶解有过量的碳酰肼和 GTX 起爆药,为 了最大限度地消除母液中溶解的碳酰肼,运用容量滴定分析法和控制变量法研究了过碳酸钠(SPC)与碳酰肼(CHZ)的反应过程和 影响因素,获得二者在 80 ℃下的最佳反应工艺条件为: CHZ(0.1 mol·L<sup>-1</sup>)和 SPC(0.15 mol·L<sup>-1</sup>)溶液的体积比为 1:4,反应时 间不少于 90 min 时, CHZ 的去除率可高达 68%。应用最小二乘法对获得的反应时间与剩余 CHZ 浓度的数据进行一级动力学和二 级动力学拟合,结果表明 CHZ 和 SPC 的反应过程符合二级动力学模型。

关键词:碳酰肼(CHZ);过碳酸钠(SPC);滴定分析。

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